

Assessment of quality of self-compacting concrete using ultrasonic pulse velocity method

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Abstract:

Due to rapid industrialization and urbanization, the demand for usage of electricity is increasing at an alarming rate. At the same time, fly ash and pond ash is produced in thermal power plant in large quantity. Fly ash is used as an alternative material in construction industries while pond ash is disposed-off on huge land areas. This study focuses on assessing the quality of self-compacting concrete (SCC) incorporating pond ash by using ultrasonic pulse velocity method which is non-destructive testing method of concrete. Fine aggregate is replaced by pond ash in percentages of 10, 15, 20, 25 and 30 in SCC. This research aims to study the influence of pond ash as a fine aggregate on quality of SCC. The compressive strength of SCC tested at 7, 28 and 90 days of curing. At 90 days of curing UPV testing was done to check the quality of SCC. The results revealed that as pond ash percentage increases UPV values decreases. The strength of mixes increases with decreasing UPV value concluded to check the durability properties.

Key Word: Self compacting concrete; Pond ash; UPV; Compressive strength; Fine aggregate.

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I. Introduction

Non-destructive determination of the compressive strength of concrete is a huge goal for researchers. Currently, the rebound number and ultrasonic pulse velocity (UPV) are recognized as two true non-destructive methods for estimating concrete strength in a structure. Unlike the rebound number technique, which measures concrete properties near the surface, the UPV technique yields information about the concrete throughout the thickness of a structural member that is accessible from two opposite sides [1].

The application of the UPV technique to the evaluation of concrete strength has been widely investigated for more than 50 years. However, the heterogeneous nature of concrete makes it almost impossible to obtain a theoretically admissible relation between UPV and strength, and, as a result, the progress of this application has been hindered. Previous studies have demonstrated that it is necessary to establish an empirical relationship between UPV and compressive strength for strength estimation [2][3][4][5][6][7].

For early-age concrete, the pulse velocity increases rapidly relative to strength [8][9]. UPV is influenced by many variables, such as mixture proportions, aggregate type and quantity, age of concrete, moisture content, and so on. Unfortunately, the factors that significantly affect pulse velocity measurements may have little influence on concrete strength and vice versa. For instance, the pulse velocity of concrete with a water/cement ratio (w/c) of more than 0.5 is drastically increased by increasing the aggregate content, while little change is observed in strength. The establishment of a calibration curve between UPV and compressive strength is thus needed to obtain a reliable estimation of concrete strength with the pulse velocity method [6].

Several previous studies [2][3][6][7][10] have concluded that, for concrete with a particular mixture proportion, there is a good correlation between UPV and strength measured at different ages. However, for concretes with a wide variety of mixture proportions, the paired data of UPV and strength are widely distributed in a scatter plot. Consequently, no clear rules have been established to describe how the relationship between UPV and concrete compressive strength changes with mixture proportion.

A step towards a better interpretation of the relationship was reported for hardened saturated concrete [11]. The coarse aggregate content was a ruling factor in establishing a UPV–strength relationship for concrete with various mixture proportions. The established relationship curves were verified to be suitable for the estimation of the strength of hardened saturated concrete with a measured UPV value. Here in this research work, a new material pond ash is introduced as a partial replacement of fine aggregate in SCC. The influence of pond ash on compressive strength is studied with the help of a linear relationship between UPV value and compressive strength.

II. Material And Methods

The Self-compacting concrete occupies all the space in the formwork without any external efforts. The most common form of concrete consists of Portland cement, coarse aggregate, sand, and water. The following materials were used for preparing SCC trial mixes with superplasticizer in this research.

Ordinary Portland cement 53 grade was used for making the concrete specimens. Ordinary Portland cement of 53 Grade conforming to IS 269-2015 was used in the study.

The manufactured aggregate is available in abundant quantity, so it was used in order to minimize the cost of SCC. For this research work, coarse aggregate having a size of 12 mm was used. Crushed sand was used as a fine aggregate.

Pond ash is a combination of fly ash and bottom ash; thus, pond ash can be used as a filler material with very little pozzolanic property [8][2][9][10]. Pulverized pond ash from Rattan India Power Ltd. Amravati, Maharashtra was used for trial mixes.

A minimum dose of PCE based superplasticizer gives better performance in the fresh state and hardened state of SCC [11]. Auramix 350 was used as a superplasticizer that is PCE-based.

In this study, pond ash was replaced with sand in self-compacting concrete. The purpose was to assess the performance of pond ash as a fine aggregate in SCC in terms of the quality of SCC. The physical properties of all materials and mechanical properties of all trial mixes were determined by some tests during the experimental work. Experimental analysis was done with reference to fresh and mechanical properties of SCC such as flowability, passing ability using IS 1199:2019 and compressive strength using IS 456:2000 (Reaffirmed in 2021) by addition of pond ash in the SCC was conducted. In this study, the slump flow test was conducted for flowability and segregation of SCC, L-box test for passing ability of SCC, and the compressive strength of M30 SCC measured using a compression test machine at 7, 28, and 90 days of curing period. Compressive strength tests were done at 7, 28 and 90 days with percentages of 0, 10, 15, 20, 25 and 30 pond ash for fine aggregate replacement [10].

Using the basic test results, concrete mix design was done considering severe exposure conditions as per IS 456:2000 and proportioning method as per IS 10262:2019 for Grade M30, with different percentages of fine aggregate replacement [12][13]. Mix proportions obtained are given in Table no.1. The compressive strength of all trial mixes prepared with increasing percentage replacement of sand by pond ash are tabulated in Table no. 2. These same cubes were used for UPV and crushing compressive strength.

UPV test is a non-destructive test method of concrete for assessing concrete quality. Onsite in the existing structure of concrete its quality is assessed without disturbing the structure. In the laboratory concrete cubes are tested for their

quality and related to compressive strength actually calculated by breaking in a compression testing machine. The cubes cured for 90 days are dried out before the test. Any suitable couplant like grease or petroleum jelly is applied

on the concrete cube's center surface and faces of the transducer for proper contact between them. The direct transmission method was used for this research work. The distance is measured between the center points of opposite faces of a cube and noted. Transducers are pressed against both faces and the ultrasonic pulse velocity meter is switched on. The traverse time is recorded. From the time taken to travel the distance and the distance recorded, velocity is calculated. Table no.3 shows IS standards for UPV values. UPV test was conducted as per the standard procedure given in IS 516-part 5 section 1. All the mixes were tested for UPV and recorded.

Table no.1 Mix IDs with percentage replacement

Sr. No.	Mix ID	Water (Kg. /m ³)	Cement (Kg. /m ³)	W/C	Pond ash % replacement	Pond ash (Kg. /m ³)	Fine aggregate (Kg. /m ³)	Coarse aggregate (Kg. /m ³)	Superplasticizer
1	T1	180	429	0.42	0	0	1029	782	1.2
2	T2	180	429	0.42	10	102.9	926.1	782	1.2
3	T3	180	429	0.42	15	154.35	874.65	782	1.2
4	T4	180	429	0.42	20	205.8	823.2	782	1.2
5	T5	180	429	0.42	25	257.25	771.75	782	1.2
6	T6	180	429	0.42	30	308.7	720.3	782	1.2

Table no. 2 Compressive strength of Mix IDs

Sr. No.	Mix ID	Compressive strength (N/mm ²)		
		7 Days	28 Days	90 days
1	T1	22.3	42.1	43.42
2	T2	23	40.42	44.56
3	T3	24.8	41.63	44.85
4	T4	25.1	43.3	43.62
5	T5	23.5	40.68	43.5
6	T6	19.42	37.92	42.79

Table no. 3 IS standards for UPV values

Sr. No.	UPV in Km/s	Concrete quality
1	>4.4	Excellent
2	3.75 to 4.40	Good
3	3.00 to 3.75	Doubtful
4	Below 3.00	Poor

III. Result and discussion

The prediction of compressive strength is shown in Table no. 4 and the corresponding correlation plots are shown in Figure no. 1. For the predicted compressive strength of different mixes, it was observed that the strength of mix T2, T3 and T5 confirmed the expected strength of that particular mix. The mixes T1, T4 and T6 fall below the estimated strength. For all SCC mixes the percentage variation did not exceed plus or minus 2.5%. In all mixes, all parameters were kept constant with percentage replacement of fine aggregate by pond ash only. Figure no. 1 shows that as the percentage of pond ash increases UPV value was decreasing up to 20% replacement that may be because of poor workmanship, or improper curing. For 25% and 30% replacement UPV value was increasing that is only because of less water cement ratio, as powder content contributing to cementitious material in the mix is increasing. Poor workmanship or improper curing results in less durable concrete with pore and capillary formation in concrete though it was having good compressive strength.

Table no.4 Predicted and Actual compressive strength of all mix IDs

Mix ID	Actual compressive strength (N/mm ²)	UPV (Km/sec)	Predicted compressive strength (N/mm ²)	Percentage variation
T1	43.42	5.3	43.61	0.43
T2	44.56	5.1	43.93	-1.43
T3	44.85	5.2	43.77	-2.47
T4	43.62	4.8	44.43	1.81
T5	43.5	5.4	43.44	-0.13
T6	42.79	5.4	43.44	1.51

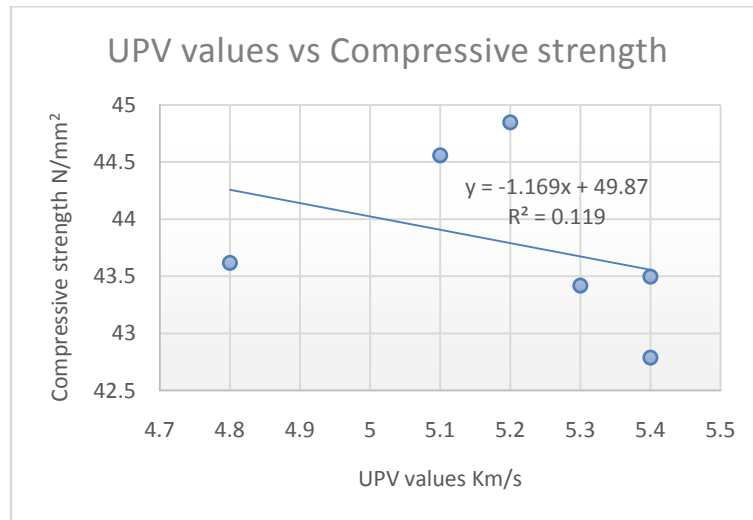


Figure no. 1 UPV values vs compressive strength

IV. Conclusion

The following conclusions have been drawn based on the results and linear regression model presented here.

1. The compressive strength of SCC increases with an increase in the percentage of pond ash up to 15% replacement. Later on, strength decreases.
2. From the results of the UPV test, negative regression is obtained. UPV is influenced by workmanship and curing conditions of mixes as all parameters were kept constant except the pond ash percentage increase.
3. As the compressive strength mixes increase UPV value is decreasing to 15%. So, durability properties need to be checked.

References

- [1]. Bungey JH, Millard SG and Grantham MG Testing of Concrete in Structures, 4th edn. Taylor & Francis, London, UK, 2006; 352.
- [2]. Andersen J and Nerenst P Wave velocity in concrete. Journal of the American Concrete Institute, 1952; 48(8): 613–636.
- [3]. Andrej G Estimate of concrete strength by ultrasonic pulse velocity and damping constant. ACI Journal, 1967; 64(10): 678–684.
- [4]. Popovics S Strength and Related Properties of Concrete: A Quantitative Approach. Wiley, New York, NY, USA, 1998.
- [5]. Popovics S, Rose LJ and Popovics JS The behaviour of ultrasonic pulses in concrete. Cement and Concrete Research, 1990; 20(2): 259–270.
- [6]. Sturup VR, Vecchio FJ and Caratin H Pulse velocity as a measure of concrete compressive strength. In Situ/Non-destructive Testing of Concrete. American Concrete Institute, Farmington Hills, MI, USA, ACI, 1984; (SP-82): 201–227.
- [7]. Tanigawa Y, Baba K and Mori H Estimation of concrete strength by combined non-destructive testing method. In Situ/non-destructive Testing of Concrete. American Concrete Institute, Farmington Hills, MI, USA, ACI, 1984; (SP-82): 57–76.
- [8]. Pessiki PS and Carino NJ Setting time and strength of concrete using the impact-echo method. ACI Materials Journal, 1988; 85(5): 389–399.
- [9]. Pessiki P and Johnson MR Non-destructive evaluation of early-age concrete strength in plate structures by the impact-echo method. ACI Materials Journal, 1996; 93(3): 260–271.
- [10]. Lin Y, Changfan H and Hsiao C Estimation of high-performance concrete strength by pulse velocity. Journal of the Chinese Institute of Engineers, 1998; 20(6): 661–668.
- [11]. Lin Y, Kuo SF, Hsiao C and Lai CP Investigation of pulse velocity–strength relationship of hardened concrete. ACI Materials Journal, 2007; 104(4): 344–350.
- [12]. M. Suthar and P. Aggarwal, “Environmental Impact and Physicochemical Assessment of Pond Ash for its Potential Application as a Fill Material,” Int. J. Geosynth. Gr. Eng., 2016
- [13]. M. P. Bhamare, Y. N. Bafna, A. K. Dwivedi, and P. Ash, “Engineering Properties of Cement CONTAINING POND ASH Properties,” IOSR J. Eng., 2012; 10(2): 7–11.
- [14]. D. S. Lal and F. Ash, “Experimental Study of Cement Mortar Incorporating Pond Ash with Elevated Temperature Exposure” International Journal of Advanced Engineering Research and Science, 2017; 6495 (5): 10–13.
- [15]. D. Lal, A. Chatterjee, and A. Dwivedi, “Investigation of properties of cement mortar incorporating pond ash – An environmental sustainable material,” Constr. Build. Mater., 2019; 209: 20–31.
- [16]. M. N. Athira Ajay, K P Ramaswamy, “A study on compatibility of superplasticizers with high strength blended cement paste,” 2020.
- [17]. IS 456 : 2000 reaffirmed 2021, “Plain and reinforced concrete - code of practice,” 2021.
- [18]. IS 10262:2019, “Concrete mix proportioning – guidelines”, January. 2019.
- [19]. IS 516-part 5- “Non-destructive Testing of Concrete”, section 1- “Ultrasonic Pulse Velocity Testing”, “Hardened concrete – methods of testing”, December 2018.