

Study of Ethanol Amine and Biodiesel in Reducing the Rate of Corrosion in Reinforced Structures

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Abstract: The properties of concrete in fresh and strengthened state were studied, while utilizing Biodiesel, Ethanol amine and blend of ethanol amine and biodiesel. The various properties of concrete were studied, through which we concluded the efficiency of corrosion inhibitors utilized (on steel). The principle part of these experiments is to get an efficient and compelling concrete inhibitor, which can inhibit corrosion. Corrosion is characterized as "The chemical reaction or action between a material, usually a metal, and its surroundings that produces deterioration of material (metal) and its properties". The outcomes we got, uncovers that ethanol amine acts as an effective corrosion inhibitor. The outcome indicates 63.41 % reduction in corrosion after 90 days of exposure in 3.5% NaCl solution without significantly changing the concrete's strength.

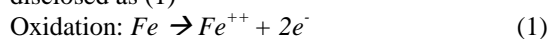
Keywords: Concrete, Inhibitor, Anodic, Cathodic etc.

I. Introduction

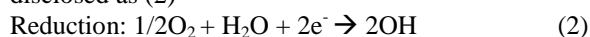
Reinforced concrete can possibly be dependable and equipped for withstanding an assortment of unfriendly conditions. Be that as it may, as an after effect of untimely support, corrosion disappointments in the structures do happen (CIP 25; Hamada, Mohammad and Otsuki *et al.*, 2003). It has turned into a genuine overall issue, with repairs cost now in the billions of dollars every year. Furthermore, the various elusive misfortunes, for example, the vitality expected to fabricate substitutions of eroded articles. The disorder spread by corrosion in scandalous. The financial misfortune and harm created by the corrosion of steel in concrete makes it possibly the biggest single infrastructural issue of modernized nations. These have tended to focus on techniques for inhibiting corrosion in concrete. Corrosion is specified as "The complicated procedure which involves chemical reaction or reactivity between a material, commonly a metal, and its surroundings that produces deterioration of material and conveys changes to various properties". Corrosion is a reaction process in which both chemical reactions and stream of electrical currents included and subsequently otherwise called electrochemical process. The steel reinforcements in concrete structures are in static conditions. They are protected by a very thin oxide layer promoted by the concrete alkalinity (pH between 12.5 to 13.5). Once the protective passivity is harmed due to chloride attack or carbonation or both, corrosion takes place (Khan *et al.*, 1991). This outcome in the development of rust having two to four times the volume of original steel and none of it has good mechanical qualities. When reinforcement corrodes, the development of corrosion product (rust) result's into weakening of bonding between concrete and steel and subsequent orientation of cracking and spalling (Al-Gahtani, Hussain & Rasheeduzzafar *et al.*, 1996). The permeable zone around the steel/concrete association can ingest higher volume of the decay products (rust) up to some degree. Some amount of decay products (rust) will diffuse into the capillary voids in the cement. However, after a while the total amount of corrosion products surpasses the quantity of corrosion products required to fill the leaky zone round the steel. The rust product can then manufacture expansive (tensile) stresses on the surrounding concrete, which lead eventually to cracking and spalling of the concrete cover.

If left unchecked, the supremacy or flawlessness of the structure can be influenced. This untimely corrosion of the steel reinforcing bars (rebars) in concrete results in failure of structure i.e. decreases the life of structures. Failure's of the structure has very high cost for maintenance, reclamation and substitution annually (Capilla, Escudero, Garcia-Alonso, Miranda, Salta & Vega *et al.*, 2007). Dissimilarities in the surface of the steel (additionally referred to as heterogeneous nature), such as contrasts in grain structure and composition and local differences in the electrolyte, due to this contradictory nature of concrete, it cause a region of the bar to act as an anode and another region to act as a cathode. On anodic sites, iron atoms lose electrons and move into the encompassing concrete as ferrous ions (anodic oxidation: Fe^{++}). The electrons travel through the bar to cathodic destinations, where they join with water and oxygen in the solid to form hydroxyl ions (OH^-). To keep up the electrical neutrality, the ferrous ions relocate through the pores of the paste to the cathode where they consolidate with hydroxyl ions to form hydrated iron oxide or rust.

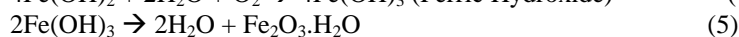
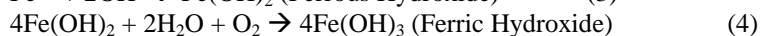
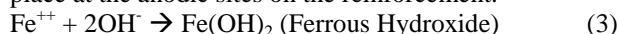
Corrosion of steel is a chemical process which incorporates both the chemical reactions and flow of electrical currents. The corrosion process is similar to the action taking place in a glimmer battery. The surface of the corroding steel works as a mixed electrode, upon which both anodic and cathodic reactions take place. Concrete pore water behaves as an aqueous medium, and it works like a convoluted electrolyte. The anodic reaction is the oxidation process (deterioration), which results in disintegration or loss of metal. Here the superficial atoms of metal lose m electrons (e^-) and pass in the electrolytic solution in the form of metal cation as indicated by the mechanism $Z \rightarrow Z^{m+} + me^-$. This stage is sometimes called anodic dissolution, which can be disclosed as (1)



The cathodic reaction (reduction process) results in reduction of dissolved oxygen forming hydroxyl ions. It is an increase of electrons (e^-) and the simultaneous incorporation of the atom formed with the crystal lattice of metal as indicated by the mechanism $Z^{m+} + me^- \rightarrow Z$. This stage is called cathodic deposition or, which can be disclosed as (2)



Some parameters are crucial to start corrosion. Presence of oxygen and humidity are the two vital parameters. On the off chance that any of these are missing, there is no corrosion. In case there is an obliged measure of water or oxygen, corrosion proceeds at a moderate rate. Humidity satisfies the electrolytic prerequisite of the corrosion cell, and moisture and oxygen together as a blend help in the formation of more OH^- thereby producing more rust component $Fe(OH)^-$. Fe^{++} ions progressively react within the pore solution to form rust. The reactions represent the formation of the product called red rust after the iron dissolution takes place at the anodic sites on the reinforcement.



Fe_2O_3 , or red rust, is the corrosion product whose volume in comparison to volume of the steel with the same mass is approximately four times. Subsequently, the development of red rust may bring internal stresses and consequently the cracking, fracturing and spalling of the concrete surrounding the reinforcement. In spite of the fact that further reactions other than specified above may occur amid the progression of the corrosion process.

II. Corrosion Inhibitor

A corrosion inhibitor can be characterized as a chemical compound, used as an admixture, either in liquid or powder form that viably diminishes or slows down reinforcement corrosion in solidified concrete if introduced, typically in small concentration. A corrosion inhibitor is an impetus chemical additive, which, when added to a corrosive aqueous environment, diminishes the rate of metal wastage. An ideally perfect corrosion inhibitor is a chemical compound that, when added in an adequate quantity to concrete can avoid or slows down corrosion of embedded steel and at the same time had no adverse effect on the properties of fresh and solidified concrete. An association named National Association of Corrosion Engineers (NACE) describes corrosion inhibitors as substance that, when added to an environment decreases or slow down the rate of attack on metal. Corrosion inhibitors interfere with the corrosion process without pernicious effects on concrete quality, however it doesn't mean that corrosion inhibitors haven't any impact except for effects on corrosion. In general, the results of an inhibitor are (1) to boost the level of chloride ion necessary to start corrosion and (2) to back of the rate of corrosion, regardless of the fact that it had already begun.

Corrosion inhibitors may include materials which mollify reinforcement corrosion by one of the following mechanisms:

1. Development of barrier layers.
2. Oxidation by passivation of the surface.
3. Influencing the environment in contact with the metal.

To be an adequate corrosion inhibitor, the chosen chemical or mixture of chemicals should meet the following requirements.

1. Promote emission of the respective electrodes at comparatively low current values.
2. The molecules should have powerful electron acceptor or donor properties or both.
3. Be compatible with the designated system so that disadvantageous side effects are not produced.
4. The solubility should be such that quick saturation of the chemical action surface occurs without being readily extracted.
5. Be compelling at the pH and temperature of the environment in which it is to be utilized.

Corrosion inhibitors can be indexed into 3 types, i.e. Anodic, Cathodic and Mixed, based on whether they interface with the corrosion reaction primarily at the anodic or cathodic or whether both are involved.

Anodic inhibitors for the most part act by forming an additive oxide film on the surface of the metal creating a huge anodic deviation of the corrosion potential. This shift or change forces the metallic surface into the passivation region. The film is originated at the anode although it may eventually cover the entire metal surface. They are also sometimes referred to as passivators. An anodic inhibitor interferes with the anodic process. Anodic inhibitors are materials that act as inhibitors because of their capacity to accept electrons. By supporting the natural passivation tendencies of metal surfaces or forming deposits that are impossible to metal ion, anodic inhibitors suppress anodic reaction. Most of the admixtures in this group are productive only when present in appreciably high concentrations. The concentration needed to suppress reaction is commonly determined by the extent of chloride to which the steel will be exposed. If an anodic inhibitor is not present at a concentration level ample enough to block off all the anodic sites, localized attack such as pitting corrosion can become a genuine problem. Few examples of anodic inhibitors are chromate, nitrite, molybdate, orthophosphate, ferric cyanide, silicates etc.

Anodic inhibitors can be divided into two groups, highly oxidizing and less oxidizing. Anodic inhibitors strengthen the protective oxide layer outside the steel which otherwise would breakdown within the sight of chloride ion. Cathodic inhibitors are normally less compelling than the anodic inhibitors. Cathodic inhibitors perform by either slowing the cathodic reaction itself or specifically precipitating on cathodic areas to restrict the diffusion of reducing species to the surface. By reducing the cathodic process, inhibitors reduce the corrosion rate. The cathodic reaction (reduction process) results in decrease of dissolved oxygen forming hydroxyl ions. If the anodic reaction given in Eq.1 is the only reaction that takes place during the corrosion process, there would be no cracking or fracturing and spalling of the concrete neighbouring the steel. However, Fe^{2+} ions continue to react within the pore solution to form rust. The reactions (3 to 5) stated earlier represent the formation of the so called "red rust" after the iron dissolution appears at the anodic sites on the reinforcement. Mixed inhibitors may (at the same time) affect both anodic and cathodic processes, as there is danger of pitting while using anodic inhibitors. Therefore, it became common practice to use mixed inhibitors instead of using both anodic and cathodic inhibitors at a time in concrete. A mixed inhibitor is usually more desirable because its effect is all encompassing, shielding corrosion resulting from chloride attack as well as that due to microcells on the metal surface. Since microcell corrosion is seen as minute distances separating anodic and cathodic areas, it is possible to locate either the anodic or cathodic sites on the reinforcement. The most well-known inhibitors of this classification are the phosphates and the silicates. Calcium stearate is the example of mixed inhibitors. Meader, Marazzani & Wombacher, *et al.*, (2004) have reported the Amino alcohol (AMA) based mixed inhibitors infiltrate into the concrete and resulting formation of a protective layer and this penetration is dependent concrete quality, porosity and humidity. Lower rate of corrosion is observed in the region where the inhibitor has infiltrated. There were no determinable properties observed neither in fresh nor in solidified concrete. Inhibitor can be applied to the concrete that contains up to 1% chloride ions by weight of cement at the extent or depth of the reinforcement, which is extremely useful for repairable structures.

2.1 Ethanol Amine as inhibitor

As reported by Gaidis, *et al.* (2004) AMA such as ethanolamine ($H_2N-CH_2-CH_2-OH$) and dimethyl-ethanolamine ($(CH_3)_2N-CH_2-CH_2-OH$) may restrict corrosion by attacking cathodic activity, blocking sites where oxygen picks up electrons and is reduced to hydroxyl ion. Gaidis also reported that mortar prisms containing 3.84% calcium nitrate, exposed to wetting and drying three times with 5% NaCl solution corrode five times slower than the reference mortar after 14 months of curing. In this paper he also stated that migrating corrosion inhibitors, based on amine carboxylate chemistry, might be utilized as admixture amid new construction or applied as a surface impregnant on existing structure. Al-Dulaijan, Al-Zahrani, Kaharaman & Saricimen, *et al.*, (2003) examined that effectiveness of a proprietary alkanolamine inhibitor (P2) that is designed to migrate through concrete to shape a defensive monolayer on the steel surface and a-water based inorganic inhibitor (Q2). The former was used as an admixture in concrete and the later was added to the batch water. Results indicate that the time –to-cracking in unadulterated concrete specimens incorporating inhibitors P2 and Q2 was higher than that in the control concrete specimens. The results indicated, Q2 is more effective than P2 in retarding corrosion in both contaminated and uncontaminated concrete.

III. Experimental Procedure

3.1 Experimental Material

The following materials were utilized as a part of the present examination.

Ordinary Portland Cement (OPC): M 20 Conforming to IS: 456-2000

Fine aggregate (FA): Betwa river sand with fineness modulus 2.027

Course aggregate (CA)

10 mm size: Well graded 10 mm coarse aggregates locally available from Dalla with fineness modulus 6.155

20 mm size: Well graded 20 mm coarse aggregates locally available from Dalla with fineness modulus 7.0444

Water: Tap water was used for preparing mortar

Mix design used: The mix design (M20) used in the present study was 1:1.11:1.02:1.53 (cement: FA:CA10:CA20) with w-c ratio (0.40) for moderate exposure as per IS:456-2000

NaCl: Tata salt was used for preparing NaCl solution with concentration of 3.5%

Steel: TATA Tiscon TMT steel was used for preparing steel embedded concrete cubes.

Chemical admixture: Ethanol amine, biodiesel and combination (1:1) of the admixtures are used as inhibitors. It was added to the concrete mix on the basis of percentage weight of cement during casting. Biodiesel was synthesized in Applied Chemistry laboratory of IPC College, Gwalior. Ethanol amine is normally commercially available.

3.2 Studies On Properties

3.2.1 Consistency

A parameter known as standard consistency is used to find out initial setting time, final setting time, soundness and strength. The standard consistency of cement paste is defined as that consistency which permits a vertical penetration for a Vicat plunger having 10 mm diameter and 50 mm length to a depth of 33-35 mm from the top of the mould. This apparatus is called Vicat apparatus and is generally used to find out the percentage of water required to produce a cement paste of standard consistency. The tests were conducted as per IS: 4031 (Part 4)-1988.

3.2.2 Setting time

Experiments for calculating initial and final setting time, as per Indian standard specification (IS: 269-1989) were carried out by Vicat apparatus.

3.2.3 Soundness Test

The soundness of cements is determined by using the expansion test with Le-Chatelier moulds according to the relevant standard. The testing of soundness of cement is of prime importance to ensure that the cement does not show any appreciable subsequent expansion. So the tests were carried out and results were recorded. Tests was carried out as per Indian standard specifications IS: 4031(Part 3)-1988.

3.2.4 Compressive strength of cement

The compressive strength of solidified cement is one of the most important properties of cement. As per the Indian standard specification (IS: 650-1991) the standard sand was used for preparing the mortar. The ration of cement and sand was kept as 1:3 and the quantity of water added in percent of combined weight of cement and sand and it was computed by the formula $P/4 + 3$. Where, P is the percentage of water required to produce cement paste of standard consistency.

3.2.5 Concrete cube specimen preparation

The test specimens of 150x150x150 mm size prismatic concrete cubes were cast for experimental studies. Three cubes of each sample were prepared. The water cement ratio was kept as 0.4 in all samples. Mixing of all samples of concrete carried out in the Structural Laboratory by using tilting drum mixer. To prepare the inhibited concrete, the inhibitor with respective percentage was added to the cement first and then this blended cement was added to fine and coarse aggregates for mixing. The cast specimens were demoulded after 24 hrs and cured in tap water for respective period of days.

3.2.6 Steel embedded concrete cube preparation

The same method, as clarified prior, was followed to prepare the different steel embedded concrete mixes. Digitally weighed 8mm dia. TMT steel bars of 50mm length were embedded in the prismatic cubes of 100 x 100 x 100 mm size by keeping 25mm cover on each side in lengthwise. Eight cubes were casted for each sample. The weight of each TMT bar was taken in grams up to three digits by using electronic weighing machine and it was recorded. The casted specimen were demolded after 24 hrs and kept in stimulated NaCl solution of 3.5% concentration for 7 days and afterward kept in dry environment for next 7 days and thus on upto 30 days and 90 days. After that, all samples were taken out of the solution and dried.

3.2.7 Synthesis of Biodiesel

Biodiesel is produced from the formation of vegetable oil. It requires a transesterification reaction, the process of changing one kind of esters into different kind of esters. Transesterification is the procedure of swapping the organic group R associated with an ester with an organic group R' of an alcohol. The finely grounded anhydrous NaOH was included into immaculate (99% or more immaculateness) methanol (20ml) in a 250 ml Erlenmeyer flask and combined energetically until all NaOH was dissolved. The immaculate vegetable oil (Soya bean) was warmed about 40°C in a 250 ml container. As the heated up oil is poured into the methoxide solution, the two layers would independent. This was mixed for 20 minutes. The contents of the flask are transferred into a 250 ml separatory funnel. The mixture will isolate into two distinctive layers. The glycerol will fall to the underneath, and the methyl esters (Biodiesel) will float on the top. Permit the experiment to sit for 60 minutes. The stopcock of the separatory funnel was opened and the glycerol was permitted to deplete into a little beaker.

Table1. Notation used for different samples

| Description of Sample | Notation |
|--|----------|
| Cement (Pure) | D1 |
| Cement + 1.5% Ethanol Amine (by cement weight) | D2 |
| Cement + 1.5% Biodiesel (by cement weight) | D3 |
| Cement + 0.75% Ethanol Amine + 0.75%Biodiesel (by cement weight) | D4 |

IV. Experimental Results

Table2. Consistency of different samples

| Sample | Consistency (%) |
|--------|-----------------|
| D1 | 30.40 |
| D2 | 28.00 |
| D3 | 30.00 |
| D4 | 29.40 |

It is observed that the required amount of water to accomplish normal consistency is more on account of blank cement paste in comparison to mixed cement with admixtures. It is changing uncertainly by utilizing admixtures. The sample with Biodiesel has more consistency than the sample with ethanol amine and sample with combination of ethanol amine and biodiesel.

Table3. Soundness of different samples

| Sample | Distance between indicator points (in mm) | | Expansion (in mm) |
|--------|---|---------------|-------------------|
| | Before Boiling | After Boiling | |
| D1 | 37 | 38 | 1 |
| D2 | 41 | 42 | 1 |
| D3 | 29 | 30 | 1 |
| D4 | 30 | 31 | 1 |

The results uncover that addition of admixtures does not influence the soundness of cement, as in all cases the expansion stayed same as 1 mm.

Table4. Setting time of different samples

| Sample | Initial Setting time in minutes | % Variation | Final Setting time in minutes | % Variation |
|--------|---------------------------------|-------------|-------------------------------|-------------|
| D1 | 78 | | 180 | |
| D2 | 83 | 6.410 | 190 | 5.556 |
| D3 | 90 | 15.384 | 191 | 6.111 |
| D4 | 86 | 10.256 | 190 | 5.556 |

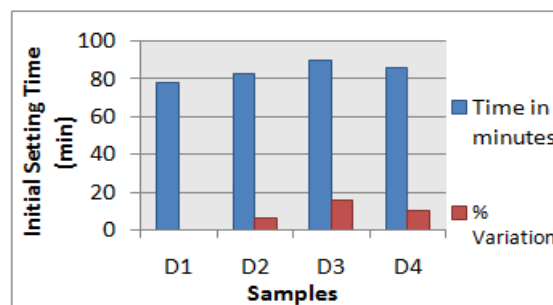


Fig. 1.1 Initial setting time of samples studied

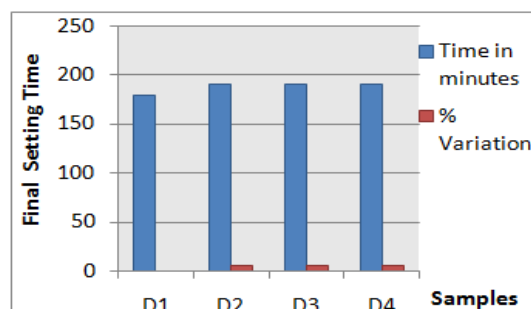


Fig. 1.2 Final Setting time of samples studied

It is observed that ethanol amine, biodiesel and their combination go about as retarders. At the point when compared the 3 samples (D2, D3, D4) it can be observed that sample with D2 ethanol amine (6.41%) trailed by D4 [50% ethanol amine, half biodiesel](10.25%) and D3 Biodiesel(15.38%). The final setting time variation stays same when compared to the pure sample.

Table5. Compressive strength of cement of different samples

| System | Compressive strength in N/mm ² | | | | | | |
|--------|---|--------|-------|--------|-------|---------|-------|
| | | 3 days | Avg. | 7 days | Avg. | 28 days | Avg. |
| D1 | 1 | 36.92 | 35.44 | 40.53 | 39.12 | 48.55 | 47.15 |
| | 2 | 34.11 | | 38.12 | | 46.14 | |
| | 3 | 35.31 | | 38.72 | | 46.75 | |
| D2 | 1 | 34.51 | 32.97 | 36.92 | 35.38 | 44.14 | 43.34 |
| | 2 | 32.50 | | 34.51 | | 43.74 | |
| | 3 | 31.90 | | 34.71 | | 42.13 | |
| D3 | 1 | 28.49 | 28.76 | 29.89 | 29.29 | 34.91 | 35.78 |
| | 2 | 28.89 | | 28.89 | | 36.11 | |
| | 3 | 28.89 | | 29.09 | | 36.31 | |
| D4 | 1 | 29.29 | 29.76 | 30.29 | 30.43 | 43.74 | 42.13 |
| | 2 | 29.89 | | 31.10 | | 40.33 | |
| | 3 | 30.09 | | 28.89 | | 42.33 | |

The obtained compressive strength of all samples after 3 days, 7 days and 28 days of curing

Table6. Variation of Compressive strength of cement of different samples

| System | Average Compressive strength in N/mm ² (3 days) | % Variation | Average Compressive strength in N/mm ² (7 days) | % Variation | Average Compressive strength in N/mm ² (28 days) | % Variation |
|--------|--|-------------|--|-------------|---|-------------|
| D1 | 35.44 | - | 39.12 | - | 47.15 | - |
| D2 | 32.97 | -6.97 | 35.38 | -9.56 | 43.34 | -8.08 |
| D3 | 28.76 | -18.85 | 29.29 | -25.10 | 35.78 | -24.11 |
| D4 | 29.76 | -16.03 | 30.43 | -22.21 | 42.13 | -10.65 |

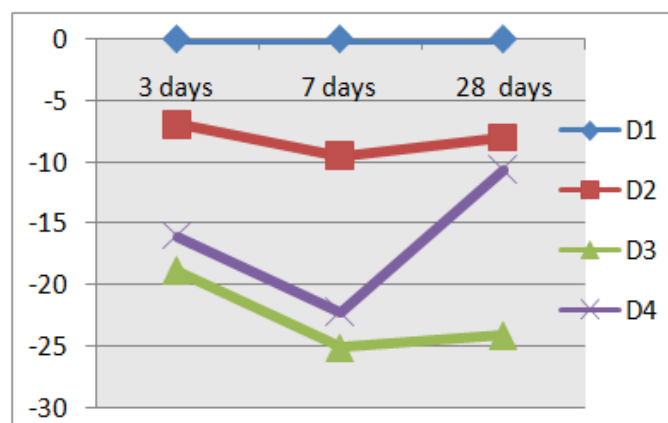


Fig. 2 Percentage variation in strength v/s Curing period of samples

It is observed that biodiesel and combination of ethanol amine and biodiesel has more impact on compressive strength of cement. The sample with ethanol amine shows comparatively less variation. The percentage deviation ranges high for the 7 days test and 28 days test compared to the 3 days. The variations in the compressive strength of the above samples are acknowledged and the combinations can be examined.

Table7. Concrete compressive strength of different samples.

| System | em | Compressive strength in N/mm ² | | | | | |
|--------|----|---|---------|---------|---------|---------|---------|
| | | 7 days | Average | 28 days | Average | 90 days | Average |
| D1 | 1 | 39.38 | 40 | 48.80 | 45.30 | 61.78 | 59.24 |
| | 2 | 39.96 | | 41.42 | | 58.49 | |
| | 3 | 40.67 | | 45.69 | | 57.47 | |
| D2 | 1 | 38.44 | 38 | 49.42 | 46.84 | 54.09 | 52.09 |
| | 2 | 36.89 | | 46.04 | | 51.33 | |

| | | | | | | | |
|----|---|-------|-------|-------|-------|-------|-------|
| | 3 | 38.67 | | 45.07 | | 50.84 | |
| D3 | 1 | 24.80 | 23.96 | 31.78 | 32.01 | 34.00 | 36.65 |
| | 2 | 23.24 | | 33.16 | | 37.38 | |
| | 3 | 23.82 | | 31.11 | | 38.58 | |
| D4 | 1 | 31.29 | 31.99 | 43.16 | 41.90 | 50.62 | 50.41 |
| | 2 | 30.93 | | 40.22 | | 48.98 | |
| | 3 | 33.73 | | 42.31 | | 51.64 | |

The compressive strength of concrete with controlled samples and the samples with ethanol amine, biodiesel and blend are observed, cured for 7, 28 and 90 days respectively

Table8. Variation of Concrete compressive strength of different samples.

| System | Average Compressive strength in N/mm ² (7 days) | % Variation | Average Compressive strength in N/mm ² (28 days) | % Variation | Average Compressive strength in N/mm ² (90 days) | % Variation |
|--------|--|-------------|---|-------------|---|-------------|
| D1 | 40.00 | - | 45.30 | - | 59.24 | - |
| D2 | 38.00 | -5.00 | 46.85 | 3.42 | 52.10 | -12.05 |
| D3 | 23.95 | -40.13 | 32.02 | -29.32 | 36.65 | -38.13 |
| D4 | 31.99 | -20.03 | 41.90 | -7.51 | 50.41 | -14.91 |

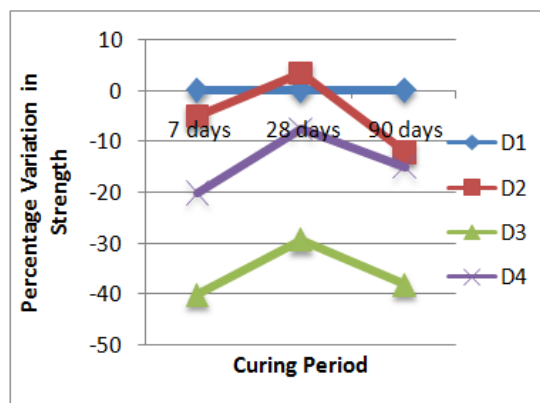


Fig. 3 Percentage variation in strength vs. Curing period of samples

For concrete specimen with blend of ethanol amine and biodiesel a reduction in the estimation of compressive strength has been distinguished as compared to control specimen. In spite of the fact that with age an expansion in compressive strength has been observed yet the values remain lower than the corresponding values of control specimen. It is also observed that the compressive strength of sample with ethanol amine at 28 days is higher than that of control sample, however later the compressive strength diminishes at the curing time of 90 days. It is also observed that the compressive strength of sample with biodiesel diminishes at higher rate when compared to the control sample.

Table9. Weight loss of bars in different samples after 30 days (steel).

| Sample | Weight of steel bars in grams before exposure | Weight of steel bars after 30 days of exposure | Wt. Loss (g) | Avg. Wt Loss | Inhibition Efficiency |
|--------|---|--|--------------|--------------|-----------------------|
| D1 | 1 | 19.730 | 19.638 | 0.092 | 0.093 |
| | 2 | 19.199 | 19.106 | 0.093 | |
| | 3 | 20.438 | 20.345 | 0.093 | |
| | 4 | 20.031 | 19.937 | 0.094 | |
| D2 | 1 | 20.002 | 19.975 | 0.027 | 0.022 |
| | 2 | 19.982 | 19.961 | 0.021 | |
| | 3 | 19.331 | 19.309 | 0.022 | |
| | 4 | 20.125 | 20.104 | 0.021 | |
| D3 | 1 | 20.954 | 20.931 | 0.023 | 0.022 |
| | 2 | 19.857 | 19.834 | 0.023 | |
| | 3 | 20.343 | 20.321 | 0.022 | |
| | 4 | 20.531 | 20.509 | 0.022 | |
| D4 | 1 | 20.341 | 20.318 | 0.023 | 0.024 |
| | 2 | 21.134 | 21.110 | 0.024 | |
| | 3 | 20.103 | 20.08 | 0.023 | |
| | 4 | 19.978 | 19.954 | 0.024 | |

Demonstrates loss of weight of implanted steel in various frameworks following 30 days in a cycle (i.e. firstly cube was immersed in 3.5 % NaCl blended water for 7 days and after that put in dry condition for next 7 days and so on). One complete cycle requires 14 days. In this way 30 days is equivalent to 2 complete cycle and 2 days.

Table10. Weight loss of bars in different samples after 90 days (steel)

| Sample | | Weight of steel bars in grams before exposure | Weight of steel bars after 30 days of exposure | Wt. Loss (g) | Avg. Wt Loss | Inhibition Efficiency |
|--------|---|---|--|--------------|--------------|-----------------------|
| D1 | 1 | 20.573 | 20.447 | 0.126 | 0.124 | |
| | 2 | 20.383 | 20.260 | 0.123 | | |
| | 3 | 20.268 | 20.145 | 0.123 | | |
| | 4 | 20.023 | 19.899 | 0.124 | | |
| D2 | 1 | 19.501 | 19.455 | 0.046 | 0.046 | 63.40 |
| | 2 | 19.144 | 19.100 | 0.044 | | |
| | 3 | 19.703 | 19.661 | 0.042 | | |
| | 4 | 20.556 | 20.505 | 0.051 | | |
| D3 | 1 | 20.081 | 20.042 | 0.039 | 0.040 | 68.29 |
| | 2 | 20.282 | 20.244 | 0.038 | | |
| | 3 | 20.094 | 20.055 | 0.039 | | |
| | 4 | 20.608 | 20.566 | 0.042 | | |
| D4 | 1 | 19.924 | 19.879 | 0.045 | 0.044 | 65.04 |
| | 2 | 19.492 | 19.449 | 0.043 | | |
| | 3 | 20.480 | 20.432 | 0.048 | | |
| | 4 | 20.885 | 20.795 | 0.040 | | |

Indicates loss of weight of implanted steel in various frameworks following 90 days (12 weeks and 6 days) in a cycle (i.e. firstly shape was drenched in 3.5% NaCl blended water for 7 days and after that set in dry condition for next 7 days et cetera). One complete cycle requires 14 days. In this manner 90 days is equivalent to 6 complete cycle and 6 days. When each sample is introduced in 3.5% NaCl solution, the inhibition efficiency continues as before for a curing time of 30 days contrasted with the controlled specimen. For the curing time of 90 days, the specimen with biodiesel has more restraint efficiency brought after by test with blend of ethanol amine and biodiesel and afterward by test with ethanol amine. Purpose behind the decrease in the erosion of the specimen is it lessens the penetrability of cement and structures a defensive layer around the steel surface.

V. Conclusions

1. Consistency of cement lessens with the expansion of inhibitors. It's (lessening in consistency) least for Biodiesel and greatest for Ethanol Amine
2. The utilization of Inhibitors increases the initial setting time of cement, accordingly they are going about as retarders. The final setting time continues as before in all samples.
3. From the studies, it can be surmised that Ethanol Amine has inhibitor proficiency of 63.4% where as in Biodiesel it is 68.04%, yet decrease in quality is more in Biodiesel.
4. Biodiesel is more successful as inhibitor, however decrease in quality is most extreme.
5. While utilizing Biodiesel, the compressive strength of cement of cement has least strength when contrasted with different inhibitors. The least compressive strength is at 7 days curing period.
6. Compared to the controlled specimen, with the exception of Ethanol Amine at 28 days the compressive strength diminishes. Most extreme lessening is in test with biodiesel.

Future Scope

- [1] Durability of reinforcement composites is a noteworthy region of research concerns. Little headway has been made in the present examination, which manages the adequacy and the productivity of Ethanol Amine, Biodiesel and blend of Ethanol Amine and Biodiesel. Examinations should be possible with expansion in the dose of Ethanol Amine and by expanding in the rate of NaCl arrangement by utilizing mixed concrete. Examinations should likewise be possible by utilizing distinctive inhibitors.
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