

A Coupled Thermoelastic Problem of A Half – Space Due To Thermal Shock on the Bounding Surface.

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I. Introduction:

This paper is concerned with the determination of temperature and displacement of a half space bounding surface due to thermal shock. This paper deals with the place boundary of the half-space is free of stress and is subjected to a thermal shock. Moreover , the perturbation method is employed with the thermoelastic coupling factor ε as the perturbation parameter. The Laplace transform and its inverse with very small thermoelastic coupling factor ε are used. The deformation field is obtained for small values of time. Paria^[7] has formulated different types of thermal boundary condition problems.

II. Formulation Of The Problem: Governing Equations

Let the elastic half-space be $x \geq 0$ with surface plane $x = 0$, free of tractions for all time. The solid is assumed to be mechanically constrained so that the displacement components $u_x = u(x, t), u_y = u_z = 0$ and the temperature distribution is of the form $T = T(x, t)$, x and t denoting respectively the space- coordinate and time.

The coupled thermo- elastic differential equations^[12] are

$$(\lambda + 2\mu) \frac{\partial^2 u}{\partial x^2} = \rho \frac{\partial^2 u}{\partial t^2} + \alpha (3\lambda + 2\mu) \frac{\partial T}{\partial x} \quad (1)$$

$$K \frac{\partial^2 T}{\partial x^2} = \rho c_\theta \frac{\partial T}{\partial t} + \alpha (3\lambda + 2\mu) \tau_0 \frac{\partial^2 u}{\partial x \partial t} \quad (2)$$

The initial conditions are taken to be

$$U(x, 0) = \frac{\partial u(x, 0)}{\partial t} = 0$$

The boundary condition is that the normal stress $\sigma_{xx}(0, t) = 0$. Introducing dimensionless variables

$$x_1 = \frac{ax}{K}, \quad t_1 = \frac{a^2 t}{K}, \quad \sigma = \frac{\sigma_{xx}}{\beta T_\phi}$$

$$T_1 = \frac{T}{T_\phi}, \quad U_1 = \frac{\alpha(\lambda + 2\mu)}{K\beta T_\phi} u,$$

$$K = \frac{K}{\rho c_\theta}, \quad a^2 = \frac{\lambda + 2\mu}{\rho}, \quad \beta = (3\lambda + 2\mu)\alpha \quad (3)$$

Equations (1) and (2) reduce to

$$\frac{\partial^2 u_1}{\partial x_1^2} = \frac{\partial T_1}{\partial x_1} + \frac{\partial^2 u_1}{\partial t_1^2} \quad (4)$$

$$\frac{\partial^2 T_1}{\partial x_1^2} = \frac{\partial T_1}{\partial t_1} + \varepsilon \frac{\partial^2 u_1}{\partial x_1 \partial t_1} \quad (5)$$

With the initial conditions

$$U_1, T_1 \frac{\partial U_1}{\partial t_1} = 0 \quad \text{at } t = 0 \text{ for all } x_1 > 0 \quad (6)$$

The boundary conditions

$$(a) \quad \sigma = \frac{\partial \sigma_{xx}}{\beta T_\phi} = \frac{\partial u_1}{\partial x_1} - T_1 = 0, \quad \text{for } x_1 = 0 \quad (7)$$

$$(b) \quad T_1 = T_0 \delta(t_1) \quad \text{for all } t_1 \geq 0$$

Due to instantaneous thermal shock on $x_1 = 0$ where T_0 is a constant and $\delta(t_1)$ is the well known Dirac – delta function.

Besides, the regularity conditions require

$$U_1, T_1, \frac{\partial U_1}{\partial x_1}, \frac{\partial T_1}{\partial x_1} \rightarrow 0 \quad \text{as } x_1 \rightarrow \infty \quad (8)$$

The constant ε represents the thermoelastic coupling factor and is given by

$$\varepsilon = \frac{\beta^2 T_0}{\rho c_\theta (\lambda + 2\mu)}$$

III. Solution Of The Problem

Let Laplace transform of $U_1(x_1, t_1)$, $T_1(x_1, t_1)$ be

$$\bar{U}_1(x_1, p) = \int_0^\infty U_1(x_1, t_1) e^{-pt_1} dt_1$$

$$\bar{T}_1(x_1, p) = \int_0^\infty T_1(x_1, t_1) e^{-pt_1} dt_1 \quad (9)$$

Laplace transform of (4) and (5) give

$$\frac{d^2 \bar{U}_1}{dx_1^2} - p^2 \bar{U}_1 = \frac{d\bar{T}_1}{dx_1} \quad (10)$$

$$\text{And } \frac{d^2 \bar{T}_1}{dx_1^2} - p \bar{T}_1 = \varepsilon p \frac{d\bar{U}_1}{dx_1} \quad (11)$$

With $\bar{U}_1(x_1, p), \bar{T}_1(x_1, p) \rightarrow 0$ as $x_1 \rightarrow \infty$

$$\bar{T}_1 = T_0 \text{ on } x_1 = 0 \quad \text{and} \quad \frac{d\bar{U}_1}{dx_1} = T_0 \text{ on } x_1 = 0 \quad (12)$$

Elimination of \bar{T}_1 from (10) and (11) gives

$$\frac{d^4 \bar{U}_1}{dx_1^4} - p(1+p+\varepsilon) \frac{d^2 \bar{U}_1}{dx_1^2} + p^3 \bar{U}_1 = 0 \quad (13)$$

Eliminating \bar{U}_1 from (10) and (11) we get the same equation in terms of \bar{T}_1

Solving these two equations satisfying first conditions of (12)

$$\bar{U}_1 = A e^{-m_1 x_1} + B e^{-m_2 x_1}$$

$$\bar{T}_1 = A_1 e^{-m_1 x_1} + B_1 e^{-m_2 x_1} \quad (14)$$

Where m_1^2 and m_2^2 are the roots of the quadratic equation

$$x^4 - p(1+p+\varepsilon)x^2 + p^3 = 0 \quad (15)$$

Hence $m_1^2 + m_2^2 = p(1+p+\varepsilon)$, $m_1^2 m_2^2 = p^3$

$$\text{And } m_1 m_2 = \frac{\sqrt{p}}{2} (\alpha_0 \pm \beta_0)$$

$$\alpha_0 = \sqrt{(1+p+\varepsilon+2\sqrt{p})}$$

$$\beta_0 = \sqrt{(1+p+\varepsilon-2\sqrt{p})}$$

Now $(\bar{T}_1)_{x_1=0} = T_0$ gives $B_1 = T_0 - A_1$

$$\text{And } \left(\frac{d\bar{U}_1}{dx_1} - T_0 \right)_{x_1=0} = 0 \text{ gives } B = -\frac{T_0 + Am_1}{m_2}$$

$$\text{Therefore } \bar{T}_1 = A_1 e^{-m_1 x_1} + (T_0 - A_1) e^{-m_2 x_1}$$

$$\bar{U}_1 = A_1 e^{-m_1 x_1} - \frac{T_0 + Am_1}{m_2} e^{-m_2 x_1} \quad (16)$$

Now, substituting the solutions (16) into (10),

$$\begin{aligned} & A(m_1^2 - p^2)e^{-m_1 x_1} + \left\{ \frac{T_0 + Am_1}{m_2} p^2 - (T_0 + Am_1)m_2 \right\} e^{-m_2 x_1} \\ & = -A_1 m_1 e^{-m_1 x_1} + (A_1 - T_0)m_2 e^{-m_2 x_1} \end{aligned}$$

This is satisfied if

$$A_1 m_1 = Ap^2 - Am_1^2$$

$$\text{And } m_2(T_0 - A_1) = m_2(T_0 + Am_1) - \frac{p^2(T_0 + Am_1)}{m_2}$$

Solving for A and A_1

$$A = \frac{m_1}{m_2^2 - m_1^2} T_0, A_1 = \frac{m_1^2 - p^2}{m_1^2 - m_2^2} T_0$$

$$\text{Hence, } \bar{T}_1 = T_0 \left[\frac{m_1^2 - p^2}{m_1^2 m_2^2} e^{-m_1 x_1} - \frac{m_2^2 - p^2}{m_1^2 - m_2^2} e^{-m_2 x_1} \right] \quad (17)$$

$$\bar{U}_1 = T_0 \left[\frac{m_2}{m_1^2 - m_2^2} e^{-m_1 x_1} - \frac{m_1}{m_1^2 - m_2^2} e^{-m_2 x_1} \right] \quad (18)$$

Since ε is generally very small, we expand in ascending powers of ε and retain terms up to its first power.
Hence

$$\alpha_0 = \sqrt{(\sqrt{p} + 1)^2 + \varepsilon} = (\sqrt{p} + 1) \left\{ 1 + \frac{\varepsilon}{2(\sqrt{p} + 1)^2} \right\} = (\sqrt{p} + 1) + \frac{\varepsilon}{2\sqrt{p} + 1}$$

$$\beta_0 = (\sqrt{p} - 1) + \frac{\varepsilon}{2} \frac{1}{\sqrt{p}-1}, \quad m_1 = p \left(1 + \frac{\varepsilon}{2} \frac{1}{p-1}\right), \quad m_2 = \sqrt{p} \left(1 - \frac{\varepsilon}{2} \frac{1}{p-1}\right) \quad (19)$$

$$\frac{1}{m_1^2 - m_2^2} = \frac{1}{p(p-1)} \left\{1 - \varepsilon \frac{p+1}{(p-1)^2}\right\}$$

Also, $m_1^2 - p^2 = \frac{\varepsilon p^2}{p-1}$, $m_2^2 - p^2 = \left(1 - \frac{\varepsilon}{p-1} - p\right)$

Using these approximations

$$\frac{T_1(x_1, p)}{T_0} = e^{-x_1 \sqrt{p}} + \varepsilon \left[\frac{e^{-px_1}}{p-1} + \frac{e^{-px_1}}{(p-1)^2} + \frac{x_1 e^{-\sqrt{p}x_1}}{2\sqrt{p}+1} - \frac{2-x_1}{2} \frac{e^{-x_1 \sqrt{p}}}{2} - \frac{e^{-x_1 \sqrt{p}}}{(p-1)^2} \right] \quad (20)$$

$$\frac{\bar{U}_1(x_1, p)}{T_0} = \frac{e^{-x_1 \sqrt{p}}}{\sqrt{p(p-1)}} - \frac{e^{-x_1 p}}{p-1} + \varepsilon \left[\frac{p+1}{p-1} e^{-px_1} + \frac{x_1}{2} \frac{p}{\sqrt{p}(p-1)^2} e^{-px_1} + \frac{x_1}{2} \frac{e^{-x_1 \sqrt{p}}}{(p-1)^2} - \frac{1}{2} \frac{e^{-x_1 \sqrt{p}}}{(p-1)^2} - \frac{1}{2} \frac{e^{-x_1 \sqrt{p}}}{\sqrt{p}(p-1)^2} - \frac{p+1}{\sqrt{p}(p-1)^3} e^{-x_1 \sqrt{p}} \right]$$

(21)

IV. Temperature Field

Using the *table*⁽¹⁴⁾, the temperature field is given by

$$\begin{aligned} \frac{T(x_1, t_1)}{T_0} &= \frac{x_1}{2\sqrt{\pi t_1^3}} e^{-\frac{x_1^2}{4t_1}} + \varepsilon [e^{t_1-x_1} H(t_1-x_1)] + (t_1-x_1)e^{(t_1-x_1)} H(t_1-x_1) \\ &\quad + \frac{x_1}{2} \left\{ \frac{1}{\sqrt{\pi t_1}} e^{-\frac{x_1^2}{4t_1}} - e^{x_1+t_1} \operatorname{erfc}\left(\frac{x_1}{2\sqrt{t_1}} + \sqrt{t_1}\right) - \left(1 - \frac{x_1}{2}\right) \frac{e^{t_1}}{2} \right\} \\ &\quad \times \left\{ e^{-x_1} \operatorname{erfc}\left(\frac{x_1}{2\sqrt{t_1}} - \sqrt{t_1}\right) + e^{x_1} \operatorname{erfc}\left(\frac{x_1}{2\sqrt{t_1}} + \sqrt{t_1}\right) \right\} - \\ &\quad \frac{t_1 e^{t_1}}{2} \left\{ e^{-x_1} \operatorname{erfc}\left(\frac{x_1}{2\sqrt{t_1}} - \sqrt{t_1}\right) + e^{x_1} \operatorname{erfc}\left(\frac{x_1}{2\sqrt{t_1}} + \sqrt{t_1}\right) \right\} \\ &\quad + \frac{x_1}{4} e^{t_1} \left\{ e^{-x_1} \operatorname{erfc}\left(\frac{x_1}{2\sqrt{t_1}} - \sqrt{t_1}\right) - e^{x_1} \operatorname{erfc}\left(\frac{x_1}{2\sqrt{t_1}} + \sqrt{t_1}\right) \right\} \\ &= \frac{x_1}{2\sqrt{\pi t_1^3}} e^{-\frac{x_1^2}{4t_1}} + \varepsilon F(x_1, t_1) \quad (22) \end{aligned}$$

Where

$$F(x_1, t_1) = e^{t_1-x_1} H(t_1-x_1) + (t_1-x_1)e^{t_1-x_1} H(t_1-x_1) + \frac{x_1}{2} \left\{ \frac{1}{\sqrt{\pi t_1}} e^{-x_1^2/4t_1} - \dots \right\}$$

In the temperature distribution(22), the first term on the right-hand side represents the solution of the classical heat conduction equation while the $F(x_1, t_1)$ is the perturbation due to the thermoelastic coupling coefficient ε . $F(x_1, t_1)$ is the perturbation function for temperature. It is seen that perturbation function is zero when t_1 is zero for all values of $x_1 > 0$.

V. Deformation Field

Thermoelastic deformation for small values of time is calculated when parameter p is large and the expansions are inverse powers of p . Hence using approximations (19) and expanding for large p , keeping terms upto $p^{-\frac{7}{2}}$, we obtain from (21)

$$\begin{aligned} \frac{\bar{U}(x_1, p)}{T_0} &= \left(\frac{\varepsilon x_1}{2} + 2\varepsilon - 1\right) \frac{e^{-x_1 p}}{p} + (x_1 \varepsilon + 2\varepsilon - 1) \frac{e^{-x_1 p}}{p^2} + \left(\frac{3\varepsilon x_1}{2} + \varepsilon - 1\right) \frac{e^{-x_1 p}}{p^3} + \left(x_1 \frac{\varepsilon}{2} - \frac{\varepsilon}{2}\right) \frac{e^{-x_1 \sqrt{p}}}{p^2} \\ &\quad + (x_1 \varepsilon - \varepsilon) \frac{e^{-x_1 \sqrt{p}}}{p^3} + \frac{e^{-x_1 \sqrt{p}}}{p^{\frac{3}{2}}} + \left(1 - \frac{3\varepsilon}{2}\right) \frac{e^{-x_1 \sqrt{p}}}{p^{\frac{5}{2}}} + (1 - 5\varepsilon) \frac{e^{-x_1 \sqrt{p}}}{p^{\frac{7}{2}}} \end{aligned}$$

Taking the inversion, we get, for small values of time, the deformation field

$$\begin{aligned} \frac{U_1(x_1, t_1)}{T_0} = & \left(\frac{\varepsilon x_1}{2} + 2\varepsilon - 1\right)H(t_1 - x_1) + (x_1\varepsilon + 2\varepsilon - 1)H(t_1 - x_1)(t_1 - x_1) \\ & + \left(\frac{3\varepsilon x_1}{2} + \varepsilon - 1\right)H(t_1 - x_1)\frac{(t_1 - x_1)^2}{2} + \left(\frac{x_1\varepsilon}{2} - \frac{\varepsilon}{2}\right)4t_1 i^2 \operatorname{erfc}\left(\frac{x_1}{2\sqrt{t_1}}\right) \\ & + (x_1\varepsilon - \varepsilon)(4t_1)^2 i^4 \operatorname{erfc}\left(\frac{x_1}{2\sqrt{t_1}}\right) + 2\sqrt{t_1} i \operatorname{erfc}\left(\frac{x_1}{2\sqrt{t_1}}\right) + \left(1 - 3\frac{\varepsilon}{2}\right)(4t_1)^{\frac{3}{2}} i^3 \operatorname{erfc}\left(\frac{x_1}{2\sqrt{t_1}}\right) \\ & + (1 - 5\varepsilon)(4t_1)^{\frac{5}{2}} i^5 \operatorname{erfc}\left(\frac{x_1}{2\sqrt{t_1}}\right) \end{aligned}$$

Where $i^n \operatorname{erfc}(x)$ denote the associated complementary error function of the n^{th} degree and $H(\eta)$ is the Heavy side unit function defined by

$$H(\eta) = \begin{cases} 1, & \eta > 0 \\ 0, & \eta < 0 \end{cases}$$

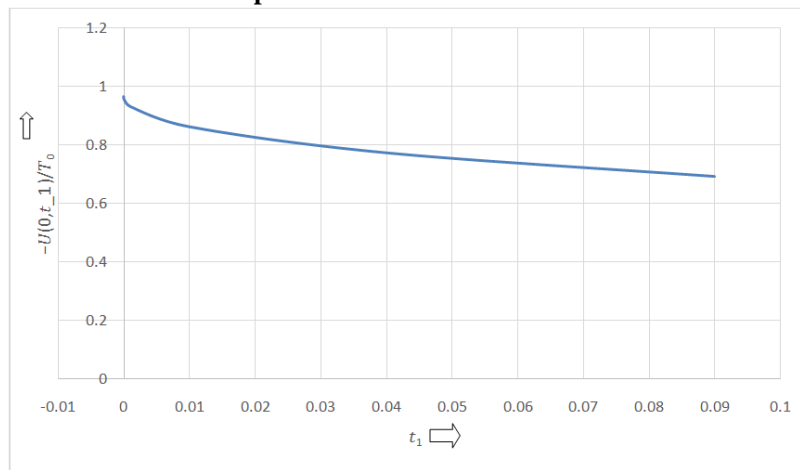
Where $x_1 = 0$ the surface displacement is

$$\begin{aligned} \frac{U(0, t)}{T_0} = & (2\varepsilon - 1)H(t_1) + (2\varepsilon - 1)H(t_1)t_1 + (\varepsilon - 1)H(t_1)\frac{t_1^2}{2} - 2\varepsilon t_1 i^2 \operatorname{erfc}(0) + 6t_1^2 \varepsilon i^4 \operatorname{erfc}(0) \\ & + 2\sqrt{t_1} i \operatorname{erfc}(0) + \left(1 - \frac{3\varepsilon}{2}\right)8t_1^{\frac{3}{2}} i^3 \operatorname{erfc}(0) + (1 - 5\varepsilon)32 t_1^{\frac{5}{2}} i^5 \operatorname{erfc}(0) \end{aligned}$$

When the material of the half space is copper, $\varepsilon = 0.0168$. The values of the surface displacement for small values of time are shown in the table:

	TABLE						
t_1	0	0.000001	0.0001	0.001	0.01	0.04	0.09
$-\frac{U(0, t_1)}{T_0}$	0.9653	0.9653	0.9552	0.9317	0.8626	0.7738	0.6932

Graphical representation of surface displacement for small values of time:



Surface displacement for small values of time

Reference

- [1] ATKINSON, K.E. (1976); A survey of Numerical Methods for the solution of Fredholm-Integral Equation of the Second – Kind Society of Industrial and applied Mathematics, Philadelphia, Pa.
- [2] CARSLAW, H.S. AND JAEGER, J.C. (1959); Conduction of heat in Solids, 2nd Edn. O.U.P.
- [3] SNEDDON, I.N. (1972); The Use of Integral Transform, McGraw Hill, New-York.
- [4] SOKOLNIKOFF, I.S. (1956); Mathematical theory of Elasticity, McGraw Hill Book Co.
- [5] WASTON, G.N. (1978); A Treatise on the Theory of Bessel Functions, 2nd Edn. C.U.P.
- [6] NOWACKI, W. (1986); Thermoelasticity, 2nd Edn. Pergamon Press.
- [7] PARIJA, G. (1968); Instantaneous heat sources in an infinite solid, India, J. Mech, Math. (spl. Issue), part I, 41.
- [8] LESSEN, M. (1968); J. Mech. Phys. Solids, 5, p.
- [9] SNEDDON, I.N. (1958); Prog. Roy. Soc. Edin. 1959, pp 121-142.
- [10] DAS, A AND DAS, B; One Dimensional Coupled Thermoelastic Problem Due To Periodic Heating In A Semi-Infinite Rod, IOSR Journal of Mathematics, Vol.3, Issue 4(Sep-Oct. 2012), pp 15-18.
- [11] LOVE, A.E.H. (1927); A Treatise on the Mathematical Theory of Elasticity, 4th Edn. Dover Publication.
- [12] NICKELL, R.E. AND SACKMAN, J.L. (1968); Approximate solution in linear coupled thermos-elasticity, J. Appl. Mech. 35, No.2, 255.
- [13] INTERNATIONAL Critical Table of Numerical data. (1927); Vol-II, N.R.C.U.S.A., McGraw Hill Book Co.
- [14] ERDELYI, A. (1954); Tables of Integral Transform, Vol-II, McGraw Hill Book Co. Inc. N.Y.